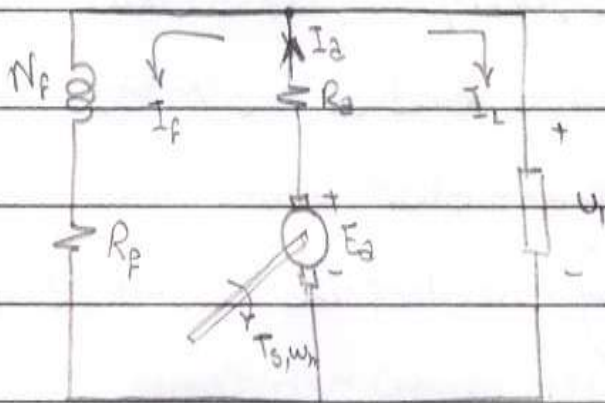


Direct Current Generator.

1. Shunt Generator.



$$P_{out} = V_t I_L \quad (\text{watt})$$

$$P_{in} = T_s \omega_m \quad (\text{watt})$$

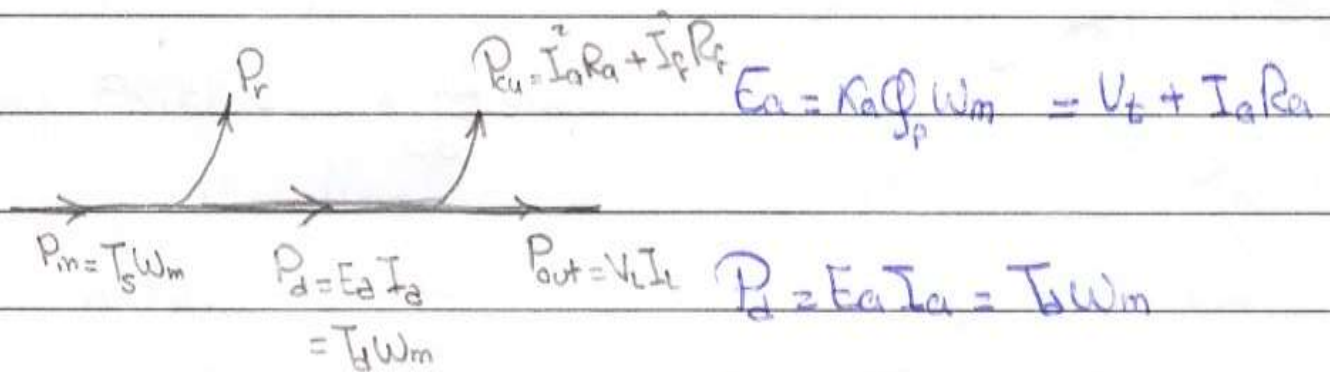
$$\omega_m = \frac{2\pi}{60} N_m \quad (\text{rad/sec})$$

equivalent ct. of shunt Gen.

$$I_a = I_f + I_L \quad (\text{Amp})$$

$$I_f = \frac{V_t}{R_f}$$

$$I_L = \frac{P_{out}}{V_t}$$



$$\eta = \frac{P_{out}}{P_{in}} \times 100\%$$

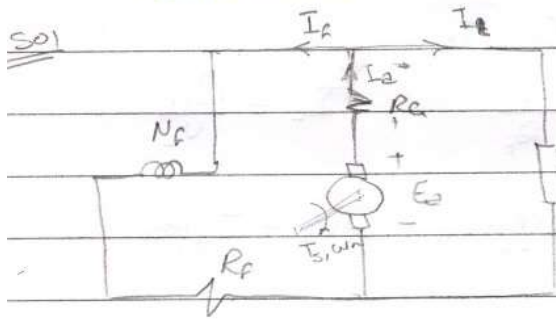
Example 2 (3-11) P. (3-40)

A 50-kW, 120 V shunt generator has $R_a = 0.09 \Omega$

$R_{fw} = 30 \Omega$, $R_{fx} = 15 \Omega$, $N_m = 900 \text{ rpm}$, $P = 5 \text{ kW}$

The generator is delivering the rated load at the rated terminal voltage. Det. a) the generator emf

T_{sh} b) torque applied c) efficiency. Neglect the armature reaction.



$$R_f = R_{fx} + R_{fw} = 30 + 15 = 45 \Omega$$

$$\omega_m = \frac{2\pi}{60} * 900 = 94.25 \text{ rad/s}$$

$$I_L = \frac{50 \times 10^3}{120} = 416.67 \text{ A}$$

$$I_f = \frac{V_L}{R_f} = \frac{120}{45} = 2.67 \text{ A}$$

$$\therefore I_a = I_f + I_L = 416.7 + 2.67 = 419.367 \text{ A}$$

$$(a) E_a = V_L + I_a R_a = 120 + (419.367 * 0.09) = 157.743 \text{ V}$$

$$(b) T_{sh} = \frac{P_{in}}{\omega_m}$$

$$P_{in} = P_r + P_a = P_r + E_a I_a = 5 \times 10^3 + (157.743)(419.367) = 71.152 \times 10^3 \text{ watt}$$

$$\therefore T_{sh} = \frac{71.152 \times 10^3}{94.25} = 754.93 \text{ N.m}$$

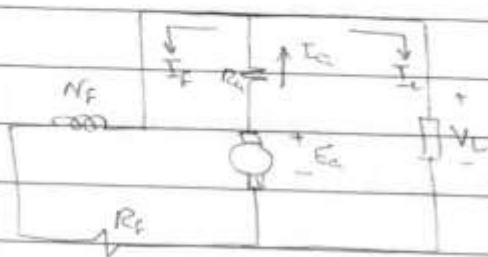
$$(c) \eta = \frac{P_o}{P_{in}} \times 100 = \frac{50 \times 10^3}{71.152 \times 10^3} \times 100 = 70.27 \% \sim 70 \%$$

A DC shunt generator driven at speed of 900 rpm. The load draw a current of 200 A for a magnetic flux per pole as 0.1 Wb. The machine parameters are armature circuit resistance = 0.1 Ω , field circuit resistance = 130 Ω , lap connected armature conductor = 300.

- draw the generator circuit and its power flow diagram for an eff. of 80%. calculate percentage voltage regulation, field and armature current, rotational and current losses, and the torque applied on the shaft.

Given:- $N_m = 900 \text{ rpm}$ $I_L = 200 \text{ A}$ $\Phi_p = 0.1 \text{ Wb}$
 $R_a = 0.1 \Omega$ $R_f = 130 \Omega$ Lap connect. $a = p$
 $Z = 300$ conductor

Sol:-

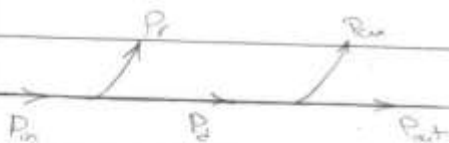


$$\omega_m = \frac{2\pi (900)}{60} = 94.25 \text{ rad/sec}$$

$$E_g = K_a \Phi_p \omega_m =$$

$$K_a = \frac{PZ}{2\pi a} = \frac{300}{2\pi} = 47.75$$

$$\therefore E_g = (47.75)(0.1)(94.25) = 450 \text{ V}$$



$$\begin{aligned} \therefore E_g &= V_L + I_a R_a \\ &= V_L + (I_L + I_f) R_a \\ 450 &= V_L + \left(I_L + \frac{V_L}{R_f}\right) R_a \end{aligned}$$

$$\eta = 80\% = \frac{P_o}{P_{in}} \times 100 =$$

$$\frac{85.93 \times 10^3}{P_{in}} = 0.8$$

$$P_{in} = 107.417 \text{ kW}$$

$$\begin{aligned} 450 &= V_L + (200 \times 0.1) + \left(\frac{0.1}{130}\right) V_L \\ 450 &= V_L + 20 + \left(\frac{0.1}{130}\right) V_L \\ 430 &= 1.000769 V_L \\ V_L &= 429.66 \text{ V} \end{aligned}$$

$$\begin{aligned} \therefore P_{out} &= V_L I_L = 429.66 \times 200 \\ &= 85.93 \text{ kW} \end{aligned}$$

$$\begin{aligned}
 * P_d &= E_a I_a = 450 \times (I_f + I_L) = 450 \left(\frac{V_L}{R_f} + 200 \right) \\
 &= 450 \left[\frac{429.99}{130} + 200 \right] \\
 &= 91.488 \text{ kW}
 \end{aligned}$$

$$\begin{aligned}
 * \text{or } P_r &= P_{in} - P_d \\
 &= 107.417 - 91.488 = 15.925 \text{ kW}
 \end{aligned}$$

$$\begin{aligned}
 * \text{U.R} &= \frac{E_a - V_t}{V_t} \times 100 = \frac{450 - 429.99}{429.99} \times 100 \\
 &= 4.653
 \end{aligned}$$

$$* I_f = V_L / R_f = 429.99 / 130 = 3.3 \text{ A}$$

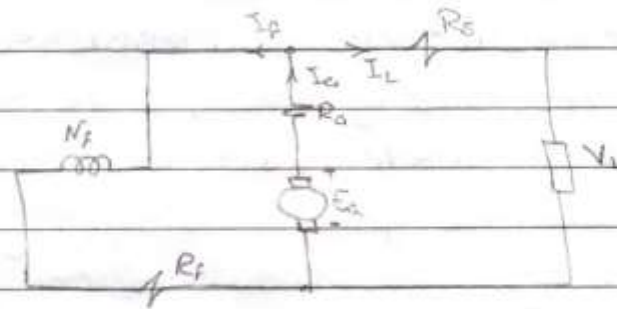
$$I_a = I_f + I_L = 3.3 + 200 = 203.3 \text{ A}$$

$$\begin{aligned}
 * P_{cu} &= I_a^2 R_a + I_f^2 R_f = (203.3)^2 (0.1) + (3.3)^2 (130) \\
 &= 4133.089 + 1422.2 \\
 &= 5.55 \text{ kW}
 \end{aligned}$$

$$* T_{sh} = \frac{P_{in}}{\omega_m} = \frac{107.417 \times 10^3}{94.25} = 1139.7 \text{ N.m}$$

* Compound Generator :-

- short shunt

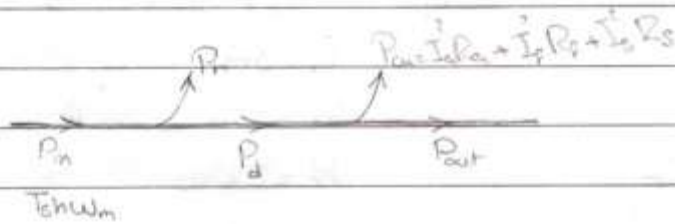


$$I_a = I_L + I_f$$

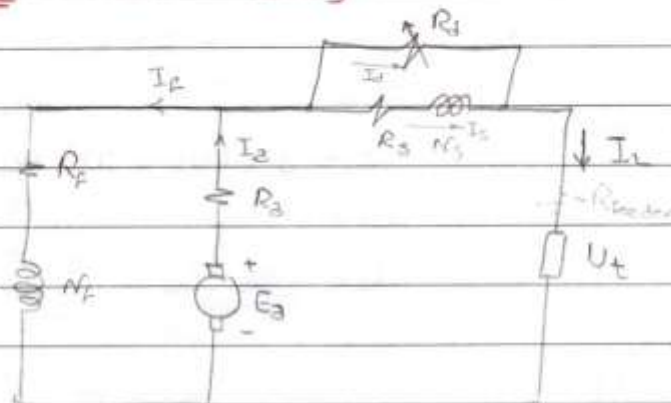
$$I_s = I_L$$

$$V_t = E_a - I_a R_a - I_s R_s$$

"equivalent ct. of short-shunt"



OR "another design"

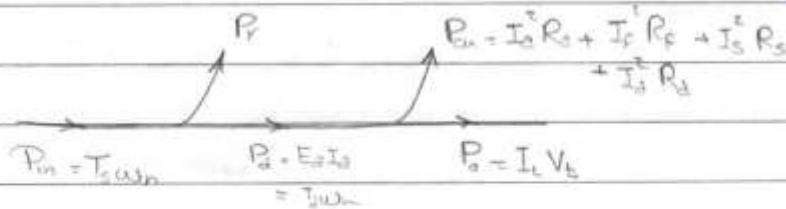


$$E_a = I_a R_a + I_s R_s + V_t + I_f R_f$$

$$E_a = I_a R_a + I_f R_f$$

$$I_a = I_L + I_f$$

$$I_s = I_L + I_f$$



deeders) (for V_t ct. series field, all V_t goes to R_{load})

$$E_a = R_a I_a + R_s I_s + I_L R_{load} + V_t$$

$$P_{cu} = I_a^2 R_{a,ind} + I_a^2 R_a + I_f^2 R_f + I_s^2 R_s + I_L^2 R_d$$

Example-

A 240V, short-shunt, cumulative compound generator is rated at 100A, the shunt field current is 3A. It has an armature resistance of 50mΩ, a series field resistance of 10mΩ, a field diverter resistance of 40mΩ, and a rotational loss of 2kW. the generator is connected to the load via a feeder R_f of 30mΩ resistance, when the generator is supplying the full load at the rated voltage, determine its efficiency. Draw the power-flow diagram to show the power distribution.

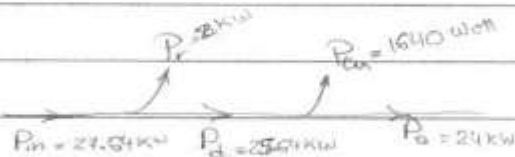
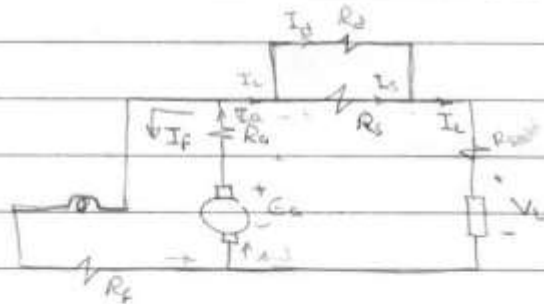
Given $V_L = 240V$ $I_L = 100A$

$I_f = 3A$ $R_a = 50m\Omega$

$R_s = 10m\Omega$ $R_d = 40m\Omega$

$P_r = 2kW$ $R_f = 30m\Omega$

$R_{fe} = 30m\Omega$



$$P_o = I_L V_L = 240 \times 100 = 24 \text{ kW}$$

$$I_a = I_f + I_L$$

$$I_a = 3 + 100 = 103 \text{ A}$$

Current divider

$$I_s = \frac{R_d I_L}{R_s + R_d} = \frac{0.04}{0.04 + 0.01} \times 100 = 80 \text{ A}$$

$$I_d = I_L - I_s = 100 - 20 = 80 \text{ A}$$

$$\therefore \eta = \frac{P_o}{P_{in}} \times 100$$

$$= \frac{24 \times 10^3}{27.64 \times 10^3} \times 100 = 93.58\%$$

$$P_a = I_a^2 R_a + I_f^2 R_f + I_s^2 R_s + I_d^2 R_d +$$

$$I_a^2 R_{fe}$$

watt

$$E_a = I_a R_a + I_s R_s + V_L + R_{fe} I_L$$

$$= (103)(0.05) + (80)(0.01) + 240 + (0.03)(100)$$

$$= 245.95 \text{ V}$$

if given N

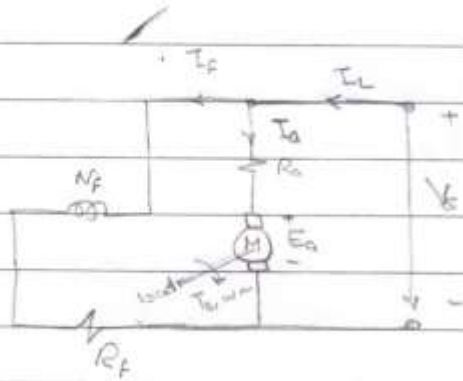
$$\therefore T_s = \frac{P_{in}}{W_n}$$

$$P_d = E_a I_a = 245.95 \times 103 = 25.64 \text{ kW}$$

$$\therefore P_{in} = P_d + P_r = 25.64 \times 10^3 + 2 \times 10^3$$

$$= 27.64 \times 10^3 \text{ watt}$$

Direct current Motor.



Back EMF

$$I_L = I_f + I_a$$

$$P_{in} = V I_L$$

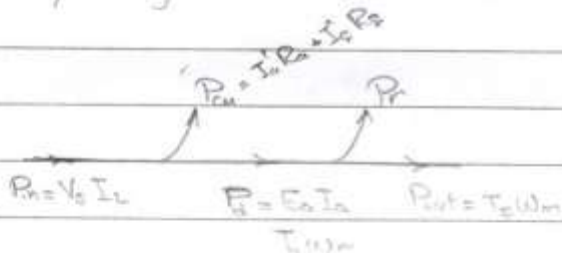
$$P_{out} = T \omega_m$$

$$V_s = I_f R_f$$

$$E_a = V_s - I_a R_a$$

$$E_a = K_a \Phi_p \omega_m$$

"eqn. of shunt motor"

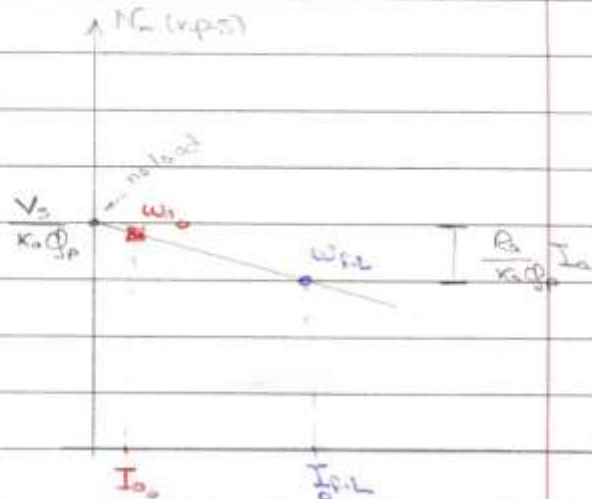


$$\omega_m = \frac{V_s - R_a I_a}{K_a \Phi_p}$$

$$V_R = \frac{V_{mload} - V_{fL} \times 100}{V_{fL}}$$

Speed regulation

$$= \frac{N_{NL} - N_{FL} \times 100}{N_{FL}}$$



Power flow diag. 1- at no load $\Rightarrow P_{out} = 0$

2- at full load $\Rightarrow P_{out} = T \omega_m$

Speed regulation

Sketch speed current char.

No load speed

$$\omega_{NL} = \frac{V_s}{K_a \Phi_p}$$

Speed drop

$$\Delta \omega = \frac{R_a}{K_a \Phi_p} I_a$$

$$I_{st} = \frac{V_s}{R_a} \text{ "starting current"}$$

See

$$\frac{E_{aNL}}{E_{aFL}} = \frac{N_{mNL}}{N_{mFL}} \text{ at const } K_a \Phi_p$$

Example (4.2) A 240 V shunt motor takes a current of 3.5 A on no load. The armature c.t. resistance is 0.5Ω and the shunt-field-winding resistance is 160Ω . When the motor operates at full load at 2400 rpm, it takes 24 A. Determine (a) Z_{FL} (b) torque developed and useful torque (T_u) (c) no-load speed (d) percent speed regulation. sketch power-flow diagram for each operating condition.

Given:- $V_s = 240 \text{ V}$ $I_L = 3.5 \text{ A}$ $R_a = 0.5 \Omega$
 $R_f = 160 \Omega$ $N_{FL} = 2400 \text{ rpm}$ $I_{FL} = 24 \text{ A}$

Sols:-

(At No-load)

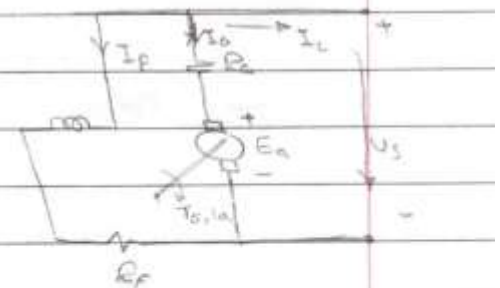
$$\therefore I_{f_{nL}} = V_s / R_f = 240 / 160 = 1.5 \text{ A}$$

$$\therefore I_a = I_L - I_f = 3.5 - 1.5 = 2 \text{ A}$$

$$E_a = V_T - I_a R_a = 240 - (2)(0.5) = 239 \text{ V}$$

$$\therefore P_d = E_a I_a = (239)(2) = 478 \text{ watt}$$

$$\therefore P_r = P_d = 478 \text{ watt} \quad \neq$$



$$P_{cu} = I_a^2 R_a + I_f^2 R_f = (2)^2(0.5) + (1.5)^2(160) = 2 + 360 = 362 \text{ watt}$$

$$\therefore P_{in} = P_{cu} + P_d = 362 + 478 = 840 \text{ watt}$$

$$P_d = T_u \omega_m$$

(at Full load)

$$I_f = 240 / 160 = 1.5$$

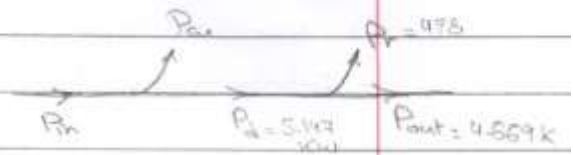
$$I_{a_{FL}} = I_L - I_f = 24 - 1.5 = 22.5 \text{ A}$$

$$E_a = V_T - R_a I_a = 240 - (0.5)(22.5) = 228.75 \text{ V}$$

$$P_a = E_a I_a = (228.75)(22.5) = 5.147 \text{ kW}$$

$$\therefore P_{out} = P_a + P_r = 5.147 \times 10^3 + 478 = 4.669 \text{ kW}$$

$$\begin{aligned} P_{cu} &= I_a^2 R_a + I_f^2 R_f \\ &= (22.5)^2 (0.5) + (1.5)^2 (160) \\ &= 613.125 \text{ watt} \\ &= P_{in} - P_d \end{aligned}$$



$$P_{in} = V_s I_L = (240)(24) = 5.76 \text{ kW}$$

$$(a) \times \eta = \frac{P_{out}}{P_{in}} \times 100 = \frac{4.669}{5.76} \times 100 = 81.06 \%$$

$$(b) \times P_d = T_d \omega_m$$

$$T_d = \frac{5.147 \times 10^3}{\frac{2\pi}{60} (2400)} = 20.48 \text{ N.m}$$

$$T_{sh} = \frac{P_{out}}{\omega_m} = \frac{4.669 \times 10^3}{\frac{2\pi}{60} (2400)} = 18.57 \text{ N.m}$$

$$\begin{aligned} (c) \quad N_{aL} &= 2400 \times \frac{E_{a nL}}{E_{a fL}} = 2400 \times \frac{239}{228.75} \\ &= 2507.54 \text{ (rpm)} \end{aligned}$$

$$\begin{aligned} (d) \quad \text{speed regulation} &= \frac{N_{aL} - N_{fL}}{N_{fL}} \times 100 = \frac{2507 - 2400}{2400} \times 100 \\ &= 4.48 \% \end{aligned}$$

20/10/2019
14/10/2019

Exercise:

(4-5) A 120V shunt motor takes 4A when it operates at ~~open~~ its no-load speed of 1200 rpm. Its armature winding resistance is 0.8Ω and the shunt field resistance is 60Ω . Determine the efficiency and the speed of the motor when it delivers its rated load of 2.4 kW.

Given:-

$$V_s = 120V$$

$$I_L = 4A$$

$$N_{n.L} = 1200 \text{ rpm}$$

$$R_a = 0.8 \Omega$$

$$R_s = 60 \Omega$$

→ at no. load

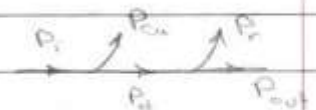
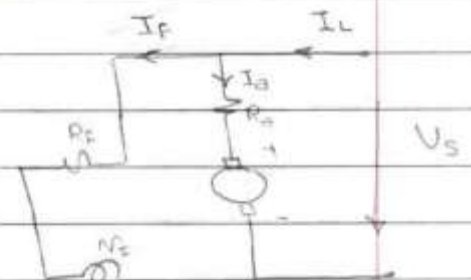
$$P_{out} = 0$$

$$\therefore P_d = P_r$$

$$P_d = E_a I_a + I_a I_L$$

$$E_a = V_s - I_a R_a$$

$$I_a = I_L = I_f$$



$$\therefore E_a = V_s - [I_L - \frac{120}{60}] 0.8$$

$$= 120 - (4 - 2) \times 0.8 = 118.4 \text{ V}$$

$$\therefore P_d = P_r = 118.4 \times 2 = 236.8 \text{ W}$$

→ At full load

$$E_{aL} = V_s - I_{aL} R_a \quad \text{V}_s = \text{constant}$$

I_{aL} is not unknown

$$P_d = I_a E_a = I_a V_s - I_a^2 R_a$$

$$P_{dL} = 120 I_{aL} - 0.8 I_{aL}^2$$

$$P_{dL} = P_r + P_{out} = 236.8 + 2.4 \times 10^3 = 2636.8$$

$$\therefore 2636.8 = 120 I_{aL} + 0.8 I_{aL}^2 = 0$$

$$I_a = 123.25$$

$$I_a = 26.7$$

rejected

$$\therefore E_a = \frac{P_{dL}}{I_{aL}} = 98.7 \approx 99 \text{ V}$$

$$\therefore I_L = I_a + I_f = 26.7 + 2 = 28.75 \text{ A}$$

$$P_m = V_s I_L = (120)(28.75) = 3450 \text{ watt}$$

$$\eta = \frac{P_{out}}{P_m} \times 100 = 69.56 \%$$

$$E_{a n.L} = \frac{N_m n.L}{N_{m f.L}}$$

$$E_{a f.L} = \frac{N_m f.L}{N_{m n.L}}$$

$$N_{m f.L} = \frac{99 \times 1200}{118.4}$$

$$= 1003.37$$

Exercise (4.6)

A 220V shunt motor draws 10A at 1800 rpm. The armature-circuit resistance is $0.2\ \Omega$, and the field-winding resistance is $440\ \Omega$. The rotational loss is 180W. Determine
 (a) back emf (b) driving torque (c) shaft torque
 (d) efficiency of the motor.

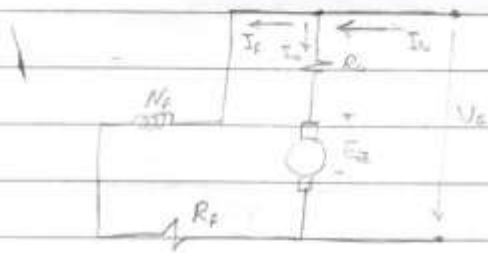
Soln:-

Given:-

$$V_s = 220\text{ V} \quad I_L = 10\text{ A} \quad N = 1800$$

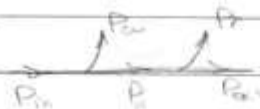
$$R_a = 0.2\ \Omega \quad R_f = 440\ \Omega$$

$$P_r = 180$$



$$\therefore I_f = V_s / R_f = \frac{220}{440} = 0.5\text{ A}$$

$$I_a = I_L - I_f = 10 - 0.5 = 9.5\text{ A}$$



$$(a) \quad E_b = V_s - I_a R_a = 220 - (9.5)(0.2) = 218.1\text{ V}$$

$$(b) \quad P_a = E_b I_a = (218.1)(9.5) = 2.07195\text{ kW}$$

$$T_a = \frac{P_a}{\omega} = \frac{2.07195 \times 10^3}{\frac{2\pi(1800)}{60}} = 10.992\text{ N.m}$$

$$P_m = V_s I_L = (220)(10) = 2200\text{ watt}$$

$$P_{out} = P_a - P_r = 2.07195 \times 10^3 - 180 = 1.89195\text{ kW}$$

$$(c) \quad \therefore T_{sh} = \frac{P_{out}}{\omega} = \frac{1.89195 \times 10^3}{\frac{2\pi(1800)}{60}} = 10.037\text{ N.m}$$

$$(d) \quad \eta = \frac{P_{out}}{P_m} \times 100 = \frac{1.89195\text{ kW}}{2200} = 85.99\%$$

A dc shunt motor drive a load for a supply voltage of 240 V. the armature current is measured as 25 A. and the rated speed is accounted to be 2200 rpm. The machine resistances are 0.8 ohm for the armature and 120 ohm for the field winding.

draw the motor circuit and its power flow diagram

calculate the machine const. $K_a \Phi_f$, the no load speed N_{nl}

the torque on the shaft for a rotational losses of 100 W

and motor efficiency.

sketch without any scale the speed current characteristics showing the rated and no load value.

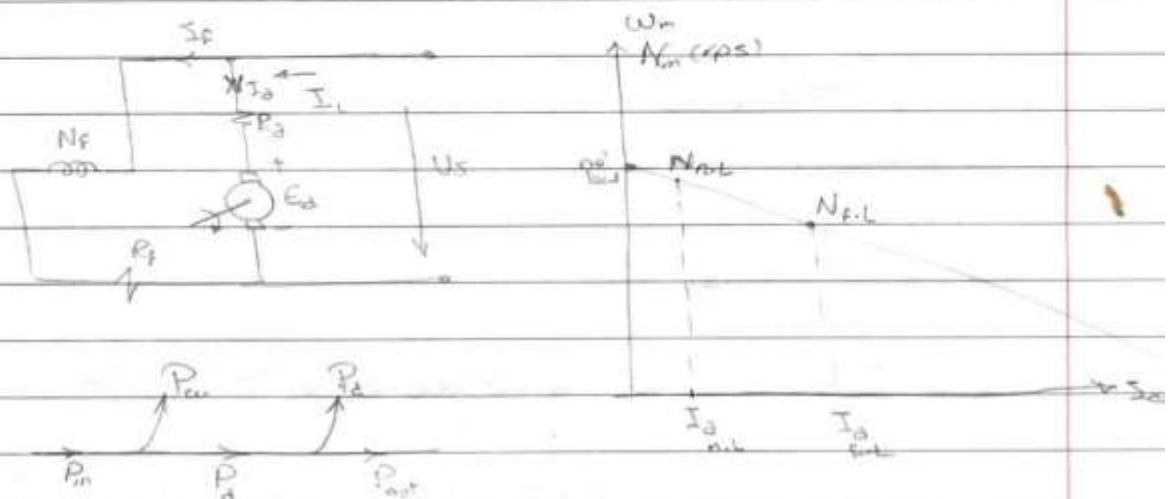
Given:- $V_s = 240V$

$I_a = 25A$

$N = 2200 \text{ rpm}$

$R_a = 0.8 \Omega$

$R_f = 120 \Omega$



$$E_a = K_a \Phi_f \omega_m = V_s - I_a R_a$$

$$K_a \Phi_f = \frac{240 - (25)(0.8)}{\frac{2\pi \times 2200}{60}} = 0.955 \text{ (V/rad/sec)}$$

$$K_a \Phi_f = 0.955 \text{ (V/rad/sec)}$$

$$\omega_m = \frac{V_s}{K_a \Phi_f} - \frac{R_a}{K_a \Phi_f} I_a$$

$$\text{at no load } \omega_m = \frac{V_s}{K_a \Phi_f} = \frac{240}{0.955} = 251.327 \text{ rad/sec}$$

P.2 المحرك rated speed $N_{r.L} \leftarrow$ rated speed

$$N_{m_{nl}} = 60 \times 251.3 / 2\pi = 2400 \text{ rpm}$$

At full load

$$P_d = E_a I_a = 220 \times 25 = 5.5 \text{ kW}$$

$$\therefore E_a = V_t - I_a R_a = 240 - (25)(0.8) = 220 \text{ V}$$

$$P_d = 220 \times 25 = 5.5 \text{ kW}$$

$$P_{out} = P_d - P_r = 5.5 \text{ kW} - 100 \text{ W} = 5.4 \text{ kW}$$

$$T_{sh} = \frac{P_{out}}{\omega} = \frac{5.4 \times 10^3}{\frac{2\pi}{60} (2400)} = 23.439 \text{ N.m}$$

$$\eta = \frac{P_{out}}{P_{in}} \times 100$$

$$P_{in} = P_{cu} + P_d$$

$$P_{cu} = I_a^2 R_a + I_f^2 R_f = (25)^2 (0.8) + \left(\frac{V_t}{720}\right)^2 120 = 500 + 480 = 980 \text{ W}$$

$$\therefore P_{in} = P_d + P_{cu} = 5.5 \times 10^3 + 980 = 6.48 \text{ kW}$$

$$\eta = \frac{5.4}{6.48} \times 100 = 84.87 \%$$

Exercise (4.7)

A 220V shunt motor draws 10A at 1800 rpm. The armature circuit resistance is 0.2Ω and the field winding resistance is 440Ω . The rotational loss is 180W.

If the torque developed by the motor is 20 N.m.

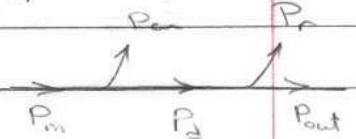
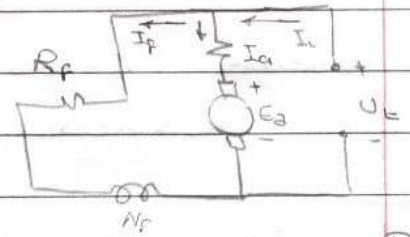
Determines- a) speed (N) b) line current (I_L)
c) efficiency.

Given: $V_t = 220V$, $I_L = 10A$

$N = 1800 \text{ rpm}$ $R_a = 0.2\Omega$

$R_f = 440\Omega$ $P_r = 180W$

$P_d = 20 \text{ N.m}$



Soln

جیبی ار T_a و T_a و T_a ال
full load
and
Power

و جیبی ال speed
at no load.

Examples:-

DC-shunt motor drive a load for supply voltage 240V. The armature current = 25A The rated speed = 2200 rpm $R_a = 0.8 \Omega$ $R_f = 120 \Omega$ calculate:-
1- Machine const. ($K_a \phi_p$)

2- N_m Int

3- $T_s \rightarrow P_r = 100W$

Given:- $V_t = 240V$ $I_a = 25A$ $N = 2200 \text{ rpm}$
 $R_a = 0.8 \Omega$ $R_f = 120 \Omega$

Sol:-

$$E_a = K_a \phi_p \omega_m$$



$$E_a = V_t - I_a R_a = 240 - (25 \times 0.8) = 220V$$

$$\therefore K_a \phi_p = \frac{E_a}{\omega_m} = \frac{220}{\frac{2\pi}{60} (2200)} = 0.9549 \text{ V(rad/sec)}$$

→ At No-load.

$$P_d = 0$$

$$\therefore P_r = P_d = E_a I_a$$

$$E_{a,nl} = V_t - I_{a,nl} R_a$$

$$P_{d,nl} = I_{a,nl} (240) - I_{a,nl}^2 (0.8)$$

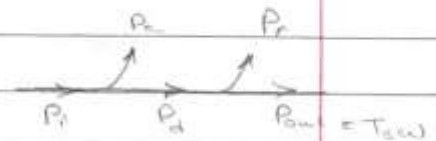
$$100 - 240 I_{a,nl} + 0.8 I_{a,nl}^2$$

$$I_a = 299.58 \text{ refused} \quad I_{a,nl} = 0.417$$

$$\therefore E_{a,nl} = 240 - (0.417 \times 0.8) = 239.66V$$

$$\therefore \frac{E_{a,nl}}{E_{a,r}} = \frac{N_{a,nl}}{N_{a,r}}$$

$$\therefore N_{a,nl} = \frac{(239.66)(2200)}{220} = 2396.66$$



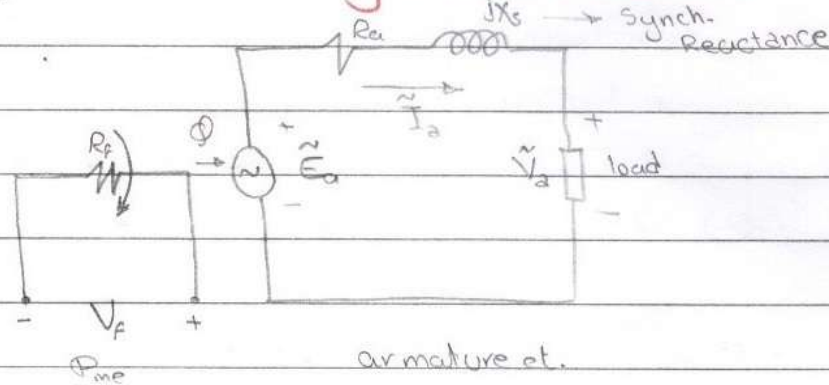
$$\therefore P_{act} = P_a - P_f = (220 \times 25) - 100 = 400 \text{ watt}$$

$$\therefore T_s = \frac{P_{act}}{\omega_{f,l}}$$

$$= \frac{400}{\frac{2\pi}{60} (2200)} = 1.736 \text{ Nm}$$

سynchronous generator

Synchronous Generator.



jX_s : Synchronous reactance

R_a : Synchronous resistance

$$\tilde{E}_a = \tilde{V}_a + \tilde{I}_a(R_a + jX_s)$$

$$\omega_s = \frac{2\pi}{60} N_s$$

$$N_s = \frac{120f}{P}$$

$$P_{in} = \omega_s T_{sh} + I_f R_f$$

$$P_d = \frac{3V_a E_a \sin \delta}{X_s}$$

$$V_a R \% = \frac{E_a - V_a}{V_a} \times 100$$

$$\eta = \frac{3V_a I_a \cos \theta}{3V_a I_a \cos \theta + P_o + 3I_a^2 R_a}$$

$$\begin{aligned} P_{in} &= T_{sh} \omega_s + I_f^2 R_f \\ &\text{or } T_{sh} \omega_s + V_f I_f \\ P_r &= I_f^2 R_f \\ P_{cu} &= 3I_a^2 R_a \\ P_d &= \frac{3E_a V_a \sin \delta}{X_s} \\ P_o &= 3V_a I_a \cos \theta \end{aligned}$$

$$\begin{aligned} P_{in} &= V_f I_f + T_{sh} \omega_m \\ P_{me} &= V_f I_f \\ P_r + P_{st} &= P_o \\ P_d &= 3I_a E_a \cos \theta \\ P_o &= 3V_a I_a \cos \theta \end{aligned}$$

$$V_{ph} = \frac{V_{line}}{\sqrt{3}}$$



V.V.I Example (2.6) :-

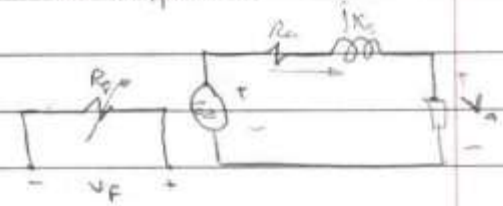
A 9-KVA, 208-V, three phase, Y-connected, synchronous generator has a winding resistance of 0.1Ω /phase and a synchronous reactance of 5.6Ω /phase. Determine its voltage regulation when the power factor of the load is (a) 80% lagging (b) unity (c) 80% leading.

Given:- $S = P = 9 \text{ K}$ $V_a = 208 \text{ V}$ Y connection

$R_a = 0.1 \Omega$ /phase $X_s = 5.6 \Omega$ /phase

Sol:-

$$\therefore V_{phase} = \frac{208}{\sqrt{3}} = 120 \text{ V}$$



$$V.R = \frac{E_a - V_t}{V_t}$$

$$E_a = V_t + I_a(R_a + jX_s) \\ = 120 + I_a(0.1 + j5.6)$$

مع تغير P.F. الـ V_t ثابت
الى بتغير هو الـ E_a

$$\rightarrow I_a = \frac{S}{3V_a} = \frac{9 \times 10^3}{3 \times 120} = 25 \text{ A}$$

بعض لما يتغير الـ P.F. حسب
الـ E_a عند كل حالة.

$$\therefore E_a = 120 + 25(0.1 + j5.6) \\ = 122.5 + j140 \text{ V}$$

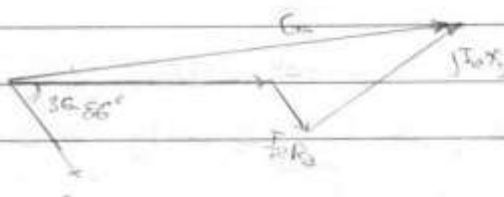
بسط الزاوية مع الـ I_a
في حساب E_a

(a) at 80% lagging

$$\therefore \text{P.F.} = 0.8 \rightarrow \theta = -36.86^\circ \quad \cos^{-1} 0.8 = 36.86^\circ$$

$$\therefore E_a = 120 + 25 \angle -36.86^\circ (0.1 + j5.6) \\ = 120 + (25 \angle 36.86^\circ)(5.6 \angle 88.97^\circ) \\ = 120 + 140 \angle 52.106^\circ = 205.988 + j110.48 \\ = 233.74 \angle 28.206^\circ \text{ V}$$

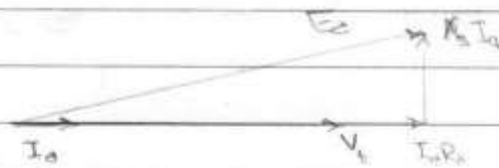
$$\therefore V.R = \frac{E_a - V_t}{V_t} = \frac{233.74 - 120}{120} \times 100 \\ = 94.8\%$$



(b) unity power factor $\theta = 0^\circ$

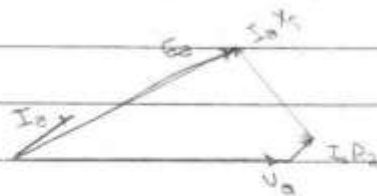
$$\begin{aligned}\tilde{E}_a &= 120 + (0.1 + j5.6) 25 \angle 0 \\ &= 122.5 + j140 = 186 \angle 48.8^\circ\end{aligned}$$

$$\therefore V.R = \frac{E_a - V_t}{V_t} \times 100 = \frac{186 - 120}{120} \times 100 = 55\%$$



(c) 80% leading - 0.8 $\theta = +36.86^\circ$

$$\begin{aligned}\therefore E_a &= V_t + 25 \angle 36.86^\circ (0.1 + j5.6) \\ &= 120 + 25 \angle 36.86^\circ (0.1 + j5.6) \\ &= 120 + (25 \angle 36.86^\circ)(5.6 \angle 88.975^\circ) \\ &= 120 + 140 \angle 125.835^\circ \\ &= 38.034 + j113.44 = 119.693 \angle 71.47^\circ \text{ V}\end{aligned}$$



$$V.R = \frac{E_a - V_t}{V_t} \times 100 = \frac{119.693 - 120}{120} \times 100$$

$$= -0.2553\%$$

في ال leading 80% +ve V.R ال leading 80% unity
في ال lagging 80% -ve V.R ال lagging 80% unity

E_a is induced emf or exciting voltage.



Given power Example (2-7)

for 3 ph

$$S = 3 \tilde{V}_a \tilde{I}_a$$

A 9 kVA, 208 V, 1200 rpm, three phase, 60 Hz, Y connected

Synchronous generator has a field winding resistance of 4.5Ω . the armature-winding impedance is $0.3 + j 5 \Omega$ /phase when the generator operates at its full load and 0.8 pf lagging the field winding current is 5 A. the rotational loss is 500 W Determine (a) the voltage regulation.

(b) efficiency of the generator

(c) the torque applied by the prime mover.

Given

$$S = 9 \times 10^3 = 3 V_a I_a$$

$$V_a = \frac{208}{\sqrt{3}} = 120 \text{ V}$$

$$R_a = 0.3 \Omega \text{ per phase} = 5 \Omega$$

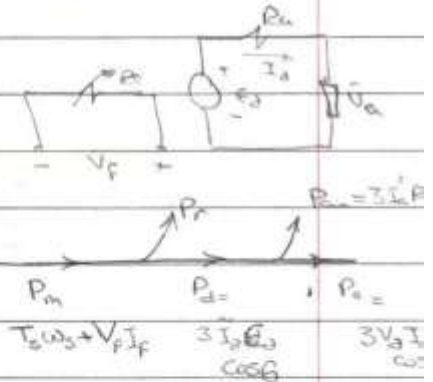
$$R_f = 4.5 \Omega$$

$$\text{PF} = 0.8 \text{ lag}$$

$$I_f = 5 \text{ A}$$

$$\theta = -36.86^\circ$$

$$P_r = 500 \text{ W}$$



Sols-

$$V_a = 120 \text{ V}$$

$$S = 3 \tilde{V}_a \tilde{I}_a$$

$$\therefore I_a = \frac{9 \times 10^3}{3 \times 120} = 25 \text{ A}$$

$$\therefore I_a = 25 \angle -36.86^\circ \text{ A}$$

$$E_a = V_t + I_a (R_a + jX_s)$$

$$= 120 + 25 \angle -36.86^\circ (0.3 + j5)$$

$$= 120 + (25 \angle -36.86^\circ) (5.186 \angle 56.31^\circ)$$

$$E_a = 120 + 125 \angle 19.45^\circ = 200.839 \angle 95.34^\circ$$

$$\therefore \text{V.R \%} = \frac{E_a - V_t}{V_t} = \frac{200.839 - 120}{120} = 67.35\%$$

$$P_o = 3 V_a I_a \cos \theta = 3 \times 120 \times 25 \times 0.8 = 7200 \text{ W}$$

$$= S \times 0.8 = 7200 \text{ W} = 7.2 \text{ kW}$$

$$\eta = \frac{P_o}{P_m} \times 100$$

$$P_m = T_a \omega_s + V_f I_f$$

$$V_f I_f = 5 \times \underbrace{(5 \times 4.5)}_{V_f} = 112.5 \text{ W}$$

$$P_d = 3 E_a I_a \cos \delta = 3(200.893)(25)(0.8) \\ = 7762.4 \text{ W}$$

$$\therefore P_{in} = P_r + P_d$$

$$T_s \omega_s = 500 + 7762.4 - 112.5 \\ = 8149.9$$

$$\therefore T_s = \frac{8149.9}{\frac{2\pi}{60} \times 1200} = 64.85 \text{ N.m}$$

$$\eta = \frac{7.2 \text{ K} \times 100}{(500 + 7762.4)} = 87 \%$$